STEAM TURBINE CALCULATION SHEET STEAM CONSUMPTION

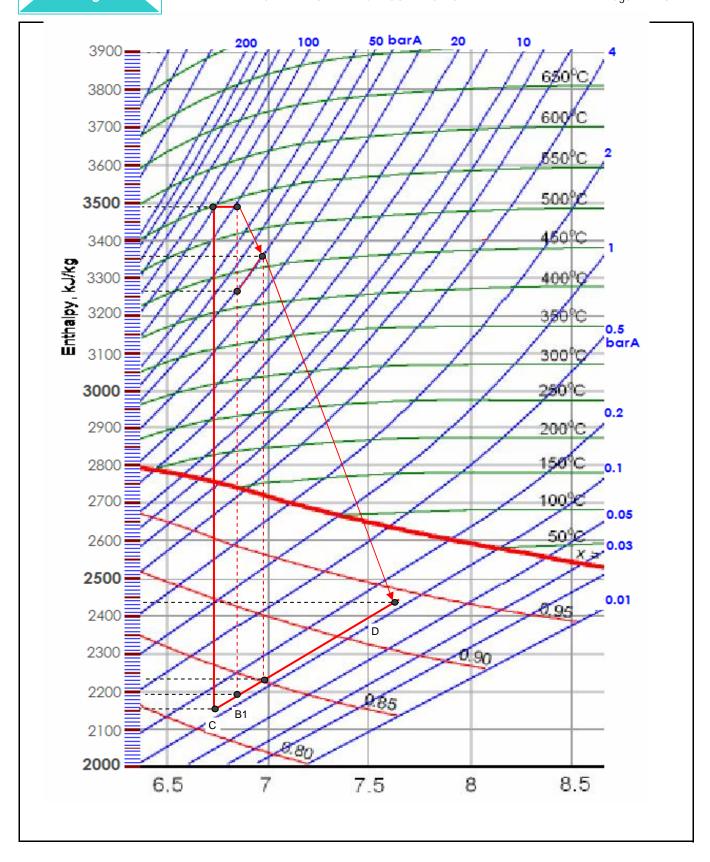
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No.	Designation		Quantity		Note and additional information
1				ON TURBINE	
2	Turbine type			REACTION	
3				age : Curtis	
4			CONDENSI	NG TURBINE	
5 6	REQUIRED CONDITION				Impulse Reaction
7	Р	kW	5500		-[3
8	N	RPM	7000		
9	pi	bar A	100		
10	ti	C	550		A desitted steem
11	Admitted pressure	bar A	40		Admitted steam
12	Admitted steam mass flow	ton/hr	5		
13	ро	bar A	0.12		
14					
15	STEAM DATA				
16					
17	hi	kJ/kg	3490		See steam Mollier diagram, point A.
18	hos	kJ/kg	2155		See steam Mollier diagram, point B
19	Δhs	kJ/kg	1335		= hi - hos
20	Governor valve factor		0.97		Multi valve 0.97, single valve 0.93
21	Δhs'	kJ/kg	1295.0		= Gov. vlv. Factor x Δhs (equation 11)
22	hos'	kJ/kg	2195.1 80		See diagram, point D
23 24	pi' ti'	bar A C	540		
	u Vİ'	m ³ /kg			Coo atoom table at all and til
25	VI	III /kg	0.0444		See steam table at pi' and ti'
26 27	CALCULATION				
28	CALCULATION				
29	Control Stage				
30	po _{IMP}	bar A	40		
31	hos' _{IMP}	kJ/kg	3265		
32	Head, Δh' _{IMP}	kJ/kg	225		
33	Calc. diameter at best eff.	mm	506.75		
34	Selected dia., D	mm	500.0		
35	Peripheral velocity, U	m/s	183.6		Equation 1
36	Head coefficient, µ _S		6.7		· ·
37	hos' _{IMP}	kJ/kg	3265.0		=hi - Δh' _{IMP}
38	Efficiency, η_{05}	Ü	0.71		Figure 12
39	Entrance area factor, A		34		
40	Trial error of control stage power	kW	440		
41	Ixε	mm	0.474		Equation 15
42	Nozzle height, I		25		Select I so that ε within the range below
43	ε		0.019		0.015 - 0.45 for welded, min. 0.07 reaming
44	Efficiency factor FI		0.93		Figure 13
45	Efficiency factor Fe		0.793		Equation in figure 13
46	Efficiency, η_{IMP}		0.52		$= \eta_{05} x F_1 x F_{\varepsilon}$

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No.	Designation		Quantity	Note and additional information
1	Δhe_{IMP}	kJ/kg	117.6	$= \eta_1 \times \Delta h_{\text{IMP}}$
2	he _{IMP}	kJ/kg	3372.4	Than make steam process in Mollier diagr.
3	Exhaust temperature, to	С	470	See steam Mollier diagram
4	Exhaust specific volume, vo	m³/kg	0.0825	See steam table
5	P _{LOSS}	kW	50.67	Equation 5
6				
7	Reaction Stages			
8	Reaction stage power	kW	5060.0 3372.4	
10	hi hos'	kJ/kg kJ/kg	2235	
11	Δhs_R	kJ/kg	1137.44	
12	Pitch diameter, D	mm	720	See fig. 11, at required speed, select pitch
13	Base diameter	mm	630	and base diameter
14	Average blade height, I	mm	90	
15	D/I		8	0.01 D Made 0.4 MD and 0.4 MD
16 17	S/I Calculated number of stages		0.40 17	=0.2 LP blade,=0.4 MP and =0.6 HP Eq. 12a (integer number)
18	Peripheral velocity, U	m/s	264.3	Eq. 12a (integer number)
19	Steam velocity, C	m/s	365.6	
20	Velocity ratio, U/C		0.72	
21	Δhs_{RSTG}	kJ/kg	66.9	
22	η_{R}		0.83	
23	Δhe_R	kJ/kg	938.38	
24	he _R	kJ/kg	2434.1	
25	X		0.940	
26	Wet enthapy	kJ/kg	2720.0	
27	Wet eficiency, η_{WET}		0.991	
28	Mechanical efficiency, η_m		0.978	
29	Turbine efficiency, η		0.80	$= \eta_R \times \eta_m \times \eta_{WET}$
30	Required steam mass flow	ton/hr	20.02	
31 32	<u>Trial result</u>			
33	Mass flow for control stage	ton/hr	15.03	Trial power of control stage until mass flow for
34	Mass flow for reaction stages	ton/hr	15.02	control stage and reaction stages minus adm.
35	minus admision steam			flow is almost equal
36				



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No.	Designation		Quantity		Note and additional information
1 2 3 4	Turbine type		ADMISSION TURBINE RATEAU+REACTION Control stage : Rateau CONDENSING TURBINE		
5	REQUIRED CONDITION		CONDENSI	NO TORDINE	
6					
7	P	kW	12000		
8	N pi	RPM bar A	6000 100		
10	ti	С	550		
11	Admitted pressure	O	40		
12	Admitted steam mass flow	ton/hr	10		
13	ро	bar A	0.12		
14					
15	STEAM DATA	1. 1/1	2400		Constant Mallian dia mana malah A
16 17	hi hos	kJ/kg	3490 2155		See steam Mollier diagram, point A. See steam Mollier diagram, point B
18	Δhs	kJ/kg kJ/kg	1335		= hi - hos
19	Governor valve factor	KJ/Kg	0.97		Multi valve 0.97, single valve 0.93
20	Δ hs'	kJ/kg	1294.95		= Gov. vlv. Factor x Δhs (equation 11)
21	hos'	kJ/kg	2195.05		See diagram, point D
22	pi'	bar Å	80		
23	ti'	С	540		
24	vi'	m³/kg	0.0444		See steam table at pi' and ti'
25					
26	CALCULATION				
27	Control Stage				
28	po _{IMP}	bar A	40		
29	hos' _{IMP}	kJ/kg	3265		
30	Head, ∆h' _{IMP}	kJ/kg	225		
31	Selected dia., D	mm	700		
32	Peripheral velocity, U	m/s	220.3		Equation 1
33	Number of stage, z		2		
34	Head coefficient, μ_S		2.3		
35	Efficiency, η_{05}		0.82		
36	Entrance area factor, A		34		
37	Trial error of control stage power	kW	1250		
38	X E	mm	1.197		Equation 15
39 40	Nozzle height, I		25 0.048		Select I so that ε within the range below 0.015 - 0.45 for welded, min. 0.07 reaming
40	ε Efficiency factor FI		0.048		Figure 13
42	Efficiency factor Fe		0.900		Equation in figure 13
43	Efficiency, η _{IMP}		0.713		$= \eta_{05} \times F_1 \times F_{\epsilon}$
44	Δhe_{IMP}	kJ/kg	160.5		$= \eta_{\text{IMP}} X \Delta h'_{\text{IMP}}$
45	·· √IMP	Northy	100.5		· IIMA · IMA
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No.	Designation		Quantity	Note and additional information
1	he _{IMP}	kJ/kg	3329.5	Than make steam process in Mollier diagr.
2	Exhaust temperature, to	С	450	See steam Mollier diagram
3	Exhaust specific volume, vo	m³/kg	0.08	See steam table
4	P _{LOSS}	kW	127.70	Equation 5
5				
6	Reaction Stages			
7	Reaction stage power	kW	10750.0	
8 9	hi hos'	kJ/kg kJ/kg	3329.5 2220	
10	Δhs_R	kJ/kg	1109.52	
11	Pitch diameter, D	mm	750	See fig. 11, at required speed, select pitch
12	Base diameter	mm	630	and base diameter
13	Average blade height, I	mm	120	
14	D/I		6	
15	S/I		0.40	=0.2 LP blade,=0.4 MP and =0.6 HP
16 17	Calculated number of stages Peripheral velocity, U	m/s	21 236.0	Eq. 12a (integer number)
18	Steam velocity, C	m/s m/s	324.9	
19	Velocity ratio, U/C	111/3	0.73	
20	Δhs_{RSTG}	kJ/kg	52.8	
21	η_{R}		0.880	
22	$\Delta he_R'$	kJ/kg	976.38	
23	he _R	kJ/kg	2353.1	
24	Χ	-	0.925	
	Wet enthalpy	kJ/kg	2720.0	
25	Wet eficiency, η_{WET}		0.986	
26	Mechanical efficiency, η_{m}		0.995	
27	Turbine efficiency, η		0.86	$= \eta_R x \eta_m x \eta_{WET}$
28	Required steam mass flow	ton/hr	40.40	
29	Trial result			
30	Maca flaw for agetral stage	ton/h-	20.01	Trial natural of control of accountil many flow for
31 32	Mass flow for control stage Mass flow for reaction stages	ton/hr ton/hr	30.91 30.40	Trial power of control stage until mass flow for control stage and reaction stages minus adm.
33	minus admision steam	(011/111	30.40	flow is almost equal
34	minus dumision stoum			now is aimost equal

